



Dubey, P. K., Yogeswaran, N., Liu, F., Vilouras, A., Kaushik, B. K. and Dahiya, R. (2020) Monolayer MoSe<sub>2</sub>-based tunneling field effect transistor for ultrasensitive strain sensing. IEEE Transactions on Electron Devices, (doi: 10.1109/TED.2020.2982732).

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# Monolayer MoSe<sub>2</sub> based Tunneling Field Effect Transistor for Ultra-Sensitive Strain Sensing

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**Abstract**—This paper presents a detailed investigation of the impact of mechanical strain on transition metal dichalcogenide (TMD) material based tunneling field-effect transistor (TFET). First, the impact of mechanical strain on material parameters of MoSe<sub>2</sub> is calculated using the first principle of density functional theory (DFT) under meta generalized gradient approximation (MGGA). The device performance of the TMD TFET has been studied by solving the self-consistent 3D Poisson and Schrodinger equations in non-equilibrium Green's function (NEGF) framework. The results demonstrate that both  $I_{ON}$  and  $I_{OFF}$  increase with uniaxial tensile strain, however, the change in  $I_{ON}/I_{OFF}$  ratio remains small. This strain dependent performance change in TMD TFET has been utilized to design an ultra-sensitive strain sensor. The device shows a sensitivity ( $\Delta I_{DS}/I_{DS}$ ) of 3.61 for a strain of 2%. Due to the high sensitivity to the strain, these result shows the potential of using MoSe<sub>2</sub> TFET as a flexible strain sensor. Furthermore, the strained TFET is analyzed for backend circuit performance. It is observed that the speed and energy efficiency of 10 stage inverter chain based on controlled strain improve substantially in comparison to unstrained TFET.

**Index Terms**—TMD TFET, transition metal dichalcogenides, uniaxial strain.

## I. INTRODUCTION

THE flexible and stretchable electronics has attracted increasing attention due to the promise it holds for advances in various applications including health monitoring, robotics and e-skin [1]–[5]. Some of these applications demand high-performance and in this regard the modest performance of organic semiconductors based devices may be insufficient. The widely used inorganic semiconductors such as silicon (Si) based devices offer excellent performance, but owing to their brittle nature they do not offer much in terms of mechanical flexibility. Through innovative methods such as wafer or chip thinning [6] and ultra-thin electronic layers by printing Si nanowires [7],[8], there has been few attempts to overcome the above issues. However, the handling of delicate ultra-thin chips and large scale uniform printing of Si based electronic layers are still challenging tasks [9]. Meanwhile, 2D materials have emerged as potential alternatives as they offer excellent properties such as atomically thin layered structure, absence of

surface dangling bonds, superior electronic property and natural compatibility with flexible electronics [10]–[14]. Specifically, mono- and few layer of MoSe<sub>2</sub> have been regarded as a promising candidate for flexible electronics due to their excellent semiconducting behavior, a tunable band gap, better mechanical stability [15], [16]. Further, the piezoresistive effect in MoSe<sub>2</sub> [17], specially the reduction in band gap with an increase in uniaxial stretching strain, can offer new functionalities such as strain, pressure, and acceleration sensing. In fact, various transition metal dichalcogenide (TMD) materials such as MoS<sub>2</sub>, MoSe<sub>2</sub> and MoTe<sub>2</sub> show strain dependent properties. This is attractive as instead of attempting to compensate the mechanically bending induced variation, they could be exploited to develop the devices for sensing applications [18], [19]. Among these, MoS<sub>2</sub> is not suitable for tunnel FET applications due to its large band gap of 1.8 eV, which significantly reduces the band-to-band tunneling probability. Semiconducting MoTe<sub>2</sub> (2H-phase) suffers from the stability issue [15], [20]. Therefore, this is not feasible for reliable FET realization, especially under external strain. MoSe<sub>2</sub>, on the other hand, has a comparatively lower band gap (1.39 eV) than MoS<sub>2</sub>, which is more suitable for TFET application. Also, it shows a better stability in 2H-phase and thus makes a good channel material for the designing steep slope strain sensitive TFET.

Herein we present the impact of the strain on MoSe<sub>2</sub> based tunneling field-effect transistors (TFET) and its potential use for strain sensing. Compared to the conventional MOSFETs, the TFETs exhibit much steeper slope in the transfer characteristics with subthreshold swing lower than the 60 mV/decade [21]–[24]. This special property makes TFETs attractive in terms of power efficiency and hence as important building blocks for next generation of high-performance flexible and stretchable electronics. The steep slope in TFETs is attributed to the band-to-band tunneling transport mechanism instead of thermal generation-based transport. The tunneling probability ( $T$ ) of the charge carriers in TFETs is exponentially dependent on the band gap ( $E_g$ ) of the material as [21]:

This work is supported in part by the British Council and Science and Engineering Research Board (SERB) through Newton-Bhabha Mobility scheme and by Engineering and Physical Sciences Research Council (EPSRC) through Engineering Fellowship for Growth (EP/R029644/1) and Heteroprint Programme Grant (EP/R03480X/1).

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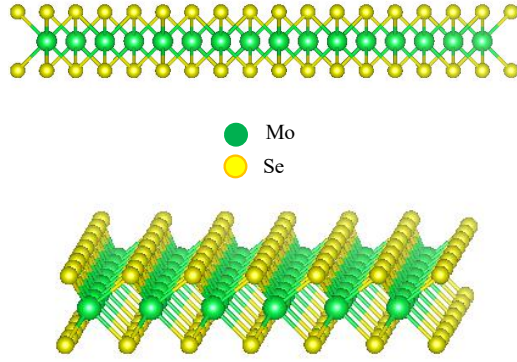


Fig. 1. Crystal structure of MoSe<sub>2</sub>.

$$T = \exp\left(-\frac{4\lambda\sqrt{2m^*}\sqrt{E_g^3}}{3q\hbar(E_g+\Delta\phi)}\right)$$

where  $m^*$  is the effective mass of the charge carrier,  $\lambda$  is the screening length and  $\Delta\phi$  is the tunneling window. The exponential dependence of the tunneling probability and tunneling current on  $E_g$  gives a unique opportunity to design ultrasensitive strain sensor using MoSe<sub>2</sub> TFET. To this end, it is important to first evaluate the impact of strain on electrical characteristics of MoSe<sub>2</sub> based TFETs. The impact of the strain on the transfer characteristics of WSe<sub>2</sub> TFET has been briefly presented in past, without much explanation about the physics behind the strain dependence of the device performance [25]. Herein, we demonstrate that the uniaxial strain impacts the band gap as well as the effective mass of the charge carrier, resulting in the strain dependent performance of MoSe<sub>2</sub> TFET. Further, we demonstrate that this strain dependence property of MoSe<sub>2</sub> TFET can be utilized to design a highly sensitive strain sensor and to improve the circuit level performance like delay and energy-delay product of the device.

This paper is arranged as follows: Section II studies the impact of uniaxial strain on the material parameters of MoSe<sub>2</sub> using the first principle density functional theory (DFT) calculation under meta generalized gradient approximation (MGGA) using the QuantumATK simulation tool [26]. Specifically, a hexagonal unit cell of MoSe<sub>2</sub> is considered for the DFT simulation with a  $k$ -point sampling of Brillouin zone along the path  $\Gamma \rightarrow M \rightarrow K \rightarrow \Gamma \rightarrow A \rightarrow L \rightarrow H \rightarrow A$  and 20 sampling point in each path (e.g. 20 sample point in  $\Gamma \rightarrow M$  path, 20 sample point in  $M \rightarrow K$  path, etc., total 140  $k$ -point). The vacuum layer is kept fixed at 10 Å. The criteria for convergence of atomic forces have been considered to be  $1 \times 10^{-6}$  Ry. The comparison of calculated electronic parameters with the literature data is presented in Table I. Then the device

Table I. Comparison of the DFT calculated electronic parameters with the literature data

Electronic parameters	Calculated value (This work)	Ref. [30]
Band gap	1.39	1.48
Effective mass of electron	0.58	0.56
Effective mass of hole	0.72	0.66

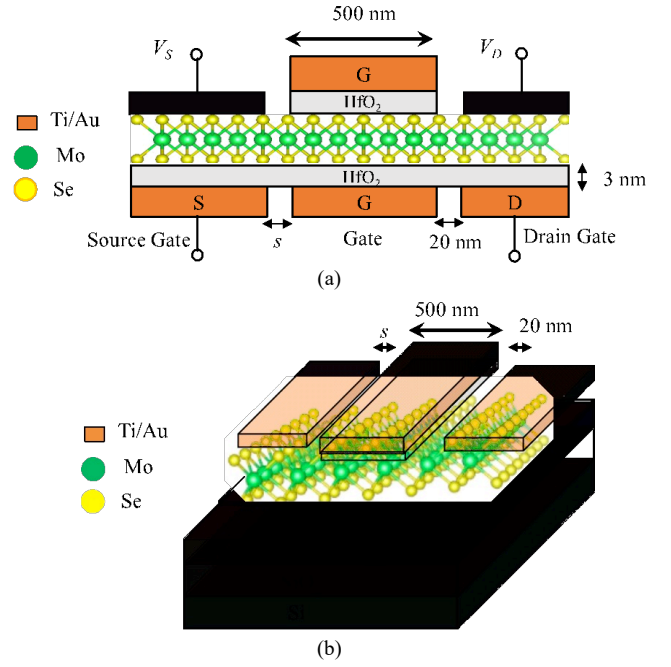


Fig. 2. (a) A 2-D schematic of MoSe<sub>2</sub> based TFET structure (b) 3-D structure of MoSe<sub>2</sub> TFET, the top and bottom gate oxide thickness is kept fixed at 3 nm..

performance at different mechanical strain conditions is studied Section III. The electrical parameters like transfer characteristics, subthreshold swing (SS) versus  $I_{DS}$  characteristics, and sensitivity of the device to the strain have been investigated. The results demonstrate that by applying a uniaxial tensile strain, the  $I_{ON}$  of TFET increases the speed and the energy efficiency of the device. The device shows a sensitivity ( $\Delta I_{DS}/I_{DS}$ ) of 3.61 for a strain of 2% that is maximum when compared with other state-of-art devices like reduced graphene oxide (rGO) FET and organic FET based strain sensors [27], [28].

## II. MATERIAL MODELING AND SIMULATION APPROACH

The device structure of MoSe<sub>2</sub> based TFET is presented in Fig. 2. The voltages of 2 V and -1V are applied to the source- and drain-gate terminals to allow doping of MoSe<sub>2</sub> under source and drain regions. The performance of MoSe<sub>2</sub> based TFET has been investigated by solving the 3D Poisson and Schrodinger equation in NEGF framework with the tight binding (TB) Hamiltonian. Two band Hamiltonian parameters of the MoSe<sub>2</sub> has been calculated using electron effective mass ( $m_e$ ), hole effective mass ( $m_h$ ) and energy band gap ( $E_g$ ). The value of  $m_e$ ,  $m_h$  and  $E_g$  of MoSe<sub>2</sub> in relax condition is considered as  $0.58 m_0$ ,  $0.72 m_0$ , and 1.39 eV, respectively. All device simulations were performed using an open source simulation tool NanoTCAD ViDES [29]. The two band Hamiltonian of MoSe<sub>2</sub> can be defined as:

$$H_{MoSe_2} = \begin{bmatrix} E_C + \frac{\hbar^2 k^2}{2m_0} & tf(k) \\ tf^*(k) & E_V + \frac{\hbar^2 k^2}{2m_0} \end{bmatrix}$$

where  $E_C$  and  $E_V$  are the bottom of the conduction band and top of the valance band, respectively. The in-plane hopping energy

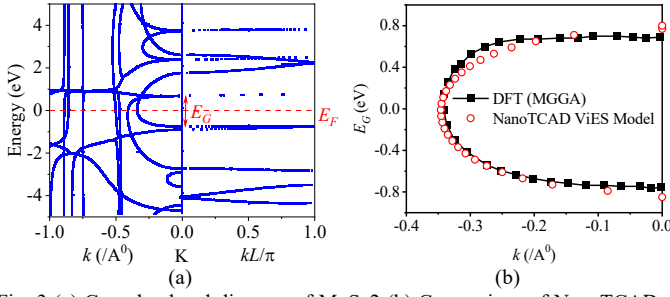


Fig. 3 (a) Complex band diagram of MoSe2 (b) Comparison of NanoTCAD ViDES model with the most relevant branch of the imaginary dispersion.

is represented by  $t$ , which depends on the effective mass and the bandgap of MoSe2 and  $f(k)$  is function due to nearest neighbor. For non-trivial solution of the crystal states of WTe2, the following conditions must be satisfied:

$$\begin{aligned} |H - E(k)I| &= 0 \\ \begin{vmatrix} E_C + \frac{\hbar^2 k^2}{2m_0} - E(k) & tf(k) \\ tf^*(k) & E_V + \frac{\hbar^2 k^2}{2m_0} - E(k) \end{vmatrix} &= 0 \end{aligned} \quad (1)$$

since in semiconductors,  $m_0$  is much larger than the effective mass of the electron that results in much smaller  $\hbar^2 k^2 / 2m_0$  in comparison to  $\hbar^2 k^2 / 2m^*$ . Therefore, it is assumed that  $\hbar^2 k^2 / 2m_0$  is negligible in comparison to  $E(k)$  and the Hamiltonian of MoSe2 reduces to the form:

$$H_{MoSe_2} = \begin{bmatrix} E_C & tf(k) \\ tf^*(k) & E_V \end{bmatrix} \quad (2)$$

where  $E_C$  and  $E_V$  are the bottom of the conduction and valence band edges,  $t$  is the in-plane hopping energy, and  $f(k)$  is a function that represents the effect of nearest neighbor. The function  $f(k)$  can be expressed as:

$$f(k) = e^{(ik_y a / \sqrt{3})} + 2e^{(-ik_y a / 2\sqrt{3})} \cos\left(\frac{k_x a}{2}\right) \quad (3)$$

where  $k_x$  and  $k_y$  are the wave vector along the  $x$ - and  $y$ -directions,  $a$  is the distance between Mo and Se atoms. Using the secular equation, the two-band dispersion relation can be

expressed as:

$$E^\pm(k) = \frac{(E_C + E_V) \pm \sqrt{(E_C - E_V)^2 + 4t^2 |f(k)|^2}}{2} \quad (4)$$

The parabolic effective mass approximation is considered with the two-band model for calculation of Hamiltonian as:

$$\frac{1}{m_R} = \frac{1}{\hbar^2} \frac{\partial^2 E^\pm(k)}{\partial k_x^2} \quad (5)$$

where  $m_R$  is the reduced mass of the electron and hole. Using Eqs. (2)-(4), and assuming the limit of second derivatives at the minimum energy  $k$ -points, the value of  $t$  can be expressed as:

$$|t|^2 = \frac{2\hbar^2 E_g}{3a^2 m_R} \quad (6)$$

where  $m_R$  is the reduced effective mass of electron and hole and can be expressed by the expression:

$$\frac{1}{m_R} = \frac{1}{m_e} + \frac{1}{m_h}$$

Solving Eq. (2), (4), and (5), we obtain the wave vector as

$$k_x = \frac{2}{a} \cos^{-1} \left( -\frac{1}{2} \cos \frac{\sqrt{3}k_y a}{2} + \sqrt{\frac{1}{4} \left( \cos^2 \frac{\sqrt{3}k_y a}{2} - 1 \right) + \frac{3a^2 m_R^*}{8\hbar^2 E_g} (E_V - E(k))(E_C - E(k))} \right) \quad (7)$$

The imaginary wave vector in the material can be expressed as:

$$\text{Im}(k_x) = \frac{2}{a} \cosh^{-1} \left( \frac{1}{\cos \frac{a \text{Re}(k_x)}{2}} \sqrt{\frac{1}{4} \left( \cos^2 \frac{\sqrt{3}k_y a}{2} - 1 \right) + \frac{3a^2 m_R^*}{8\hbar^2 E_g} (E_V - E(k))(E_C - E(k))} \right) \quad (8)$$

To validate the model for MoSe2, we have compared the imaginary  $E$ - $k$  curve obtained using (6) with the most relevant branch of the complex band structure (Fig. 3) obtained from DFT simulation under TB09 meta-GGA (MGGA) approximation. It is observed that the NanoTCAD ViDES result is consistent with the first principle DFT calculation result.

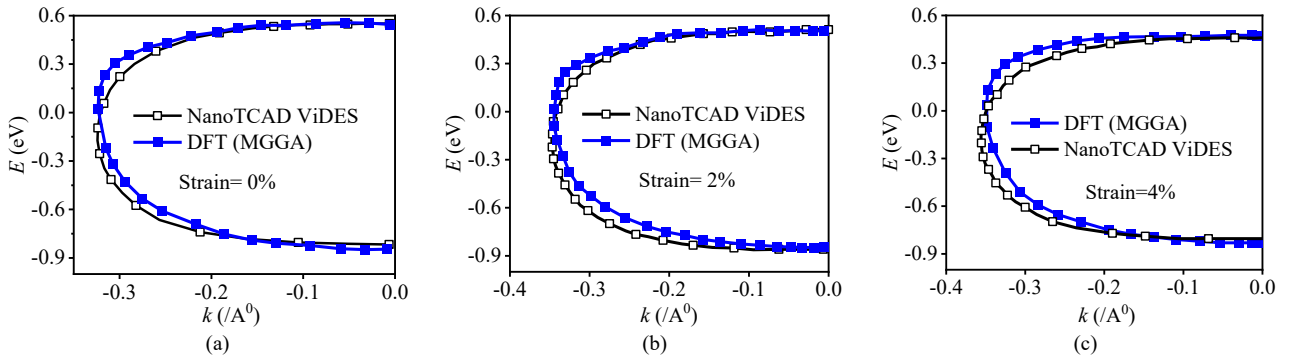


Fig. 4. Imaginary branch of  $E$ - $k$  diagram in (a) relax condition (b) in 2% strain (c) at 4% strain condition

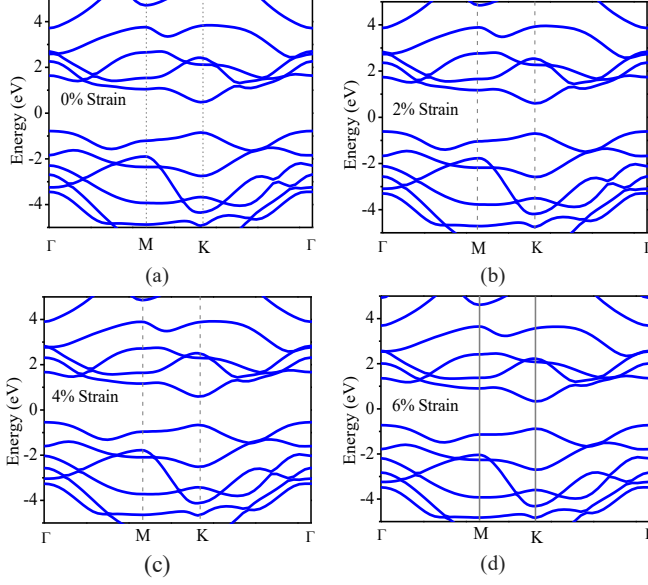


Fig. 5. Band diagram of MoSe<sub>2</sub> at strain of (a) 0% (b) 2% (c) 4% (d) 6%.

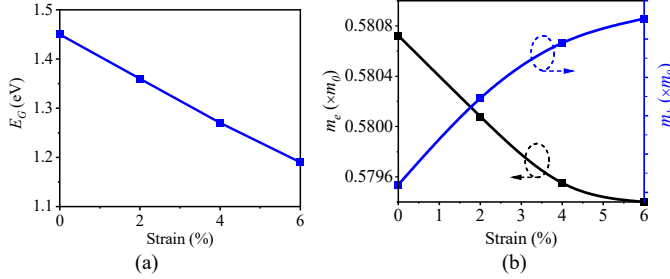


Fig. 6. Impact of strain on (a) band gap (b) electron and hole effective masses

Further, the comparison of  $E$ - $k$  curve obtained using tight binding model (7) in strained conditions and DFT calculation is presented in Fig. 4. It can be observed that the NanoTCAD results are in good agreement with the DFT results in strain conditions also. This shows that the tight-binding model is capable to capture the strain effects in the electronic structure of MoSe<sub>2</sub>.

### III. RESULTS AND DISCUSSION

The impact of the uniaxial strain on the band gap and effective masses of the semiconductor has been calculated using the first principle DFT method under MGGA approximation. The  $E$ - $k$  dispersion relation of the MoSe<sub>2</sub> under the relaxed condition, and 2%, 4%, and 6% uniaxial tensile strain conditions are presented in Fig. 5. The  $E$ - $k$  dispersion curves and their curvatures are used to calculate the band gap and effective mass of the charge carriers. The variation in energy band gap of MoSe<sub>2</sub> with a percentage change in uniaxial strain is presented in Fig. 6 (a). It can be observed that the band gap decreases linearly with an increase in the uniaxial strain. The variation of the electron and hole effective masses with strain variation is presented in Fig. 6 (b). The effective mass of electron shows a very small variation of  $0.5807m_0$  to  $0.5794m_0$  with a change in the strain from 0% to 5%, while the uniaxial strain has a dominating impact on the effective mass of hole and it changes from  $0.720m_0$  to  $1.153m_0$ . However, such variations do not

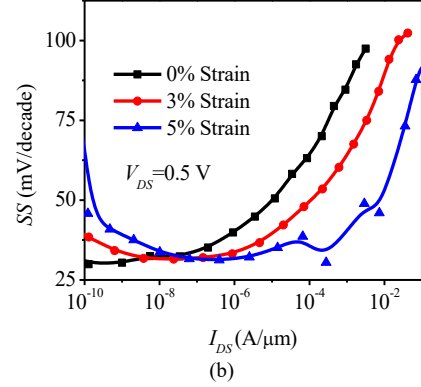
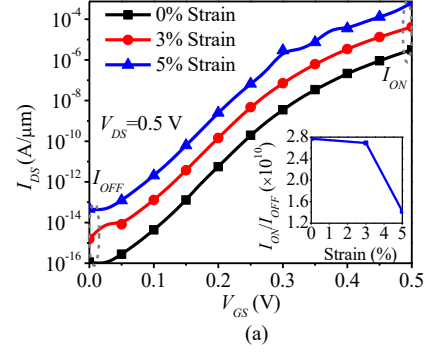


Fig. 7. Impact of strain on (a) the transfer characteristics and (b) SS versus  $I_{DS}$  characteristics of the MoSe<sub>2</sub> based TFET at  $V_{DS}=0.5$  V at a fixed  $s$  of 4 nm.

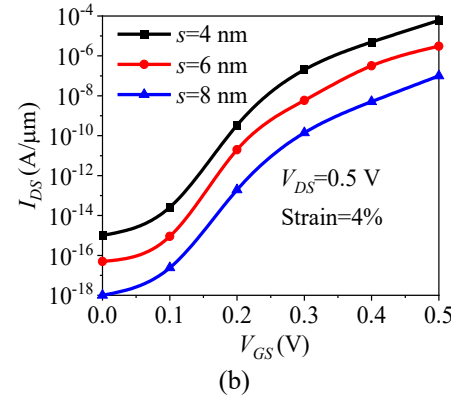
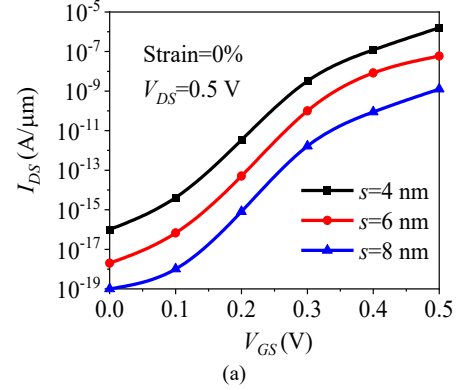


Fig. 8. Impact of source-drain metal gap ( $s$ ) on transfer characteristics in (a) zero strain and (b) 4% strain conditions

affect the performance of the device significantly since the tunneling current is dominated by electrons. As the curvature of the valence band at  $\Gamma$  point is smaller than the curvature of the conduction band at the K-point, the effective mass of the hole remains higher than the effective mass of the electron in all



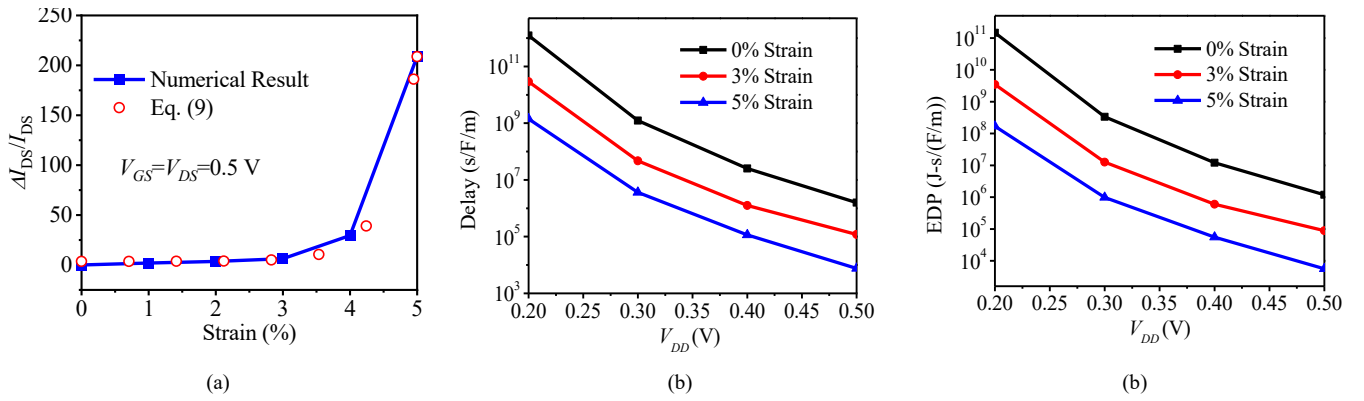


Fig.9. Impact of strain on the (a) sensitivity ( $\Delta I_{DS}/I_{DS}$ ) of the MoSe2 TFET of 10 stage inverter chain (b) delay and (c) energy-delay product of 10 stage inverter chain

strain conditions. The calculated band gap and effective masses have been used to study the device performance of TFET at different strain conditions. The impact of strain on transfer and SS versus  $I_{DS}$  characteristics are presented in Fig. 7. It can be noted that the  $I_{ON}$  and  $I_{OFF}$  increases with the increase of external strain while the  $I_{ON}/I_{OFF}$  ratio remains nearly the same (inset Fig. 7a). Such increase in the drain current with mechanical strain is attributed to the decrease in energy band gap of MoSe<sub>2</sub> as discussed previously in Fig. 5. On the other hand, the SS of MoSe<sub>2</sub> TFET at higher strain conditions remains low for a wide range of drain current. Under all the strain conditions, the SS of the device can be as low as  $\sim 25$  mV/dec, which is comparable to the best reported results so far [18]-[19], [21]-[22]. The impact of source-gate metal gap ( $s$ ) on the performance of the device in strained and zero strain conditions is presented in Fig. 8. It can be observed that the  $s$  is a crucial parameter in electrostatic doping based TFET design and need to be controlled to avoid the variability issues. The sensitivity of the device ( $\Delta I_{DS}/I_{DS}$ ) as a function of mechanical strain is presented in Fig. 9 (a). The MoSe<sub>2</sub> TFET shows a high sensitivity to the applied strain. The nonlinear variation in sensitivity of MoSe<sub>2</sub> TFET is due to the exponential dependence of TFET current on the energy band gap. By empirical curve fitting of the sensitivity versus strain curve, it is observed that the sensitivity exponentially depends on the strain ( $\epsilon$ ) as:

$$\frac{\Delta I_{DS}}{I_{DS}} = A_1 + A_2 \exp(-\epsilon/B) \quad (9)$$

where  $A_1$ ,  $A_2$  and  $B$  are constants and have values of 3.60, 0.0019 and -0.43 respectively. The Eq. (9) can also be used to determine the sensitivity of the device. A comparison of the key performance parameters of the MoSe<sub>2</sub> TFET sensor with the reported strain sensors are presented in Table II. It can be observed that the MoSe<sub>2</sub> TFET shows maximum sensitivity in

Table II. Comparison of performance parameters with reported strain sensors.

Performance Indicators	Reduced Graphene oxide FET [27]	Pentacene based Organic FET [28]	P3HT based Organic FET [28]	MoSe2 TFET (This work)
Strain	0.35%	2%	2%	2%
Sensitivity ( $\Delta I_{DS}/I_{DS}$ )	0.03	0.4685	0.08536	3.61
Operating Voltage	3 V	10 V	10 V	0.5 V

comparison to organic FET and graphene FET to the mechanical strain and operates at a comparatively lower supply voltage. In fact, the strain sensitivity of 9 times higher than the value reported for Pentacene based organic FET. These results indicate that the external strain could be used as stimuli to modulate the channel current and in this regard the presented FET could also be used as a strain sensor. The modulation of device channel current by external stimuli such as touch/contact force, temperature and even chemicals has been used in past to obtain highly sensitive physical and chemical sensors [4], [31]-[35]. Further, we have studied the impact of the strain on the performance of the TFET based 10 stage inverter chain (Fig. 9b and Fig. 9c) assuming symmetric  $n$ TFET and  $p$ TFET structures [21]. The normalized delay and energy per operation can be written as [36], [37].

$$E = V_{DD}^2 \left( \alpha + L_D \frac{I_{OFF}}{I_{ON}} \right) \quad (10)$$

where  $t_p = V_{DD} L_D / I_{ON}$  is the normalized delay of the the inverter chain,  $L_D$  is the number of stages,  $E$  is the normalized energy per operation,  $\alpha$  is the activity factor, and  $V_{DD}$  is the supply voltage. We have compared the delay versus  $V_{DD}$  and energy-delay product (EDP) versus  $V_{DD}$  characteristics of TFET in 0%, 3% and 5% strain conditions. The  $\alpha$  was fixed at 3% for a fair comparison. The speed and energy-delay product (EDP) of the circuit decreases with increase in the uniaxial mechanical strain. This improvement in delay and EDP of the inverter chain is attributed to the decrease in band gap with an increase in uniaxial mechanical strain that enhance the ON current of the device. Therefore, the circuit performance of MoSe<sub>2</sub> TFET can be potentially improved by applying a controlled mechanical strain on the device using an external force. As a single device, the proposed MoSe<sub>2</sub> TFET can be used as a strain sensor, but when put together in the circuit under controlled strain conditions they lead to high-performance and low power applications. In contrast to conventional FET technology where carrier transport is due to thermionic injection, the TFETs shows weaker dependence on the temperature variations due to band-to-band tunneling based carrier injection mechanism [38]. Therefore, the response of device is tolerant to temperature variations when used in the circuits.

#### IV. CONCLUSION

This paper investigates the impact of mechanical strain on the

MoSe<sub>2</sub> based TFET structure. The device displayed a steep slope with SS down to ~30 mV/dec. This is significantly lower than the Boltzmann limit (60 mV/decade) at room temperature and comparable to the best reported TMD based FET. With external uniaxial strain, the  $I_{ON}$  and  $I_{OFF}$  of MoSe<sub>2</sub> TFET increased with the increase in strain while the steep slope (thus SS) remains robust. With these results, the presented device shows a potential for strain sensing application with an exponential dependence between the sensitivity of the device and the applied strain. Further, the enhancement of  $I_{ON}$  under strain condition can be utilized to reduce delay and energy-delay product of TFET based circuits. A case study of strained TFET based 10-stage inverter chain clearly demonstrates an improvement of the speed and energy efficiency.

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